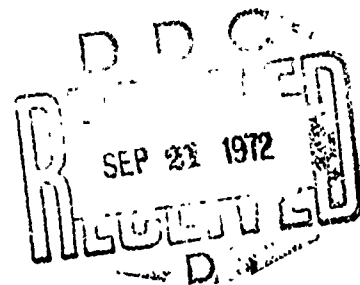


AD 748655

A FORTRAN PROGRAM FOR CALCULATING THE FREQUENCIES AND
MODE SHAPES OF AN ARBITRARY SHAPE CYLINDRICAL TYPE
SHELL BY UTILIZING A FINITE ELEMENT SOLUTION

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ABSTRACT

This report describes a Fortran IV program capable of obtaining a finite element numerical solution to the free axisymmetric vibrations of a cylindrical type shell of arbitrary shape.

INTRODUCTION

Present flextensional designs may be grouped into one of five different classes (1). In order to derive a mathematical model for any of the above mentioned flextensional transducers, it is essential to determine the vibrational characteristics of the shell itself. A finite difference approach for each shell's dynamic response has been investigated at the Center for Acoustical Studies in the Department of Mechanical and Aerospace Engineering at North Carolina State University. An attempt in improving the widely used finite difference method led to the present investigation of the finite element method which is widely used in determining stresses and strains in Aerospace Research and Development.

The program utilizes a finite element analytical model to calculate the total Mass and Stiffness matrices of an arbitrary shape cylindrical type shell (2). After the total Mass and Stiffness matrices are calculated, displacement boundary conditions are introduced by removing appropriate rows and columns corresponding to points of the shell which are rigidly restrained from motion. Finally, subroutine NROCT is used for the numerical solution of the shell's free axisymmetric vibration matrix equation, and the eigenvalues, frequency coefficients, natural frequencies, and eigenvectors are then printed out.

PROGRAM UTILIZATION

The program is written in Fortran IV (G or H level) to be used on an IBM 370/165 computer. The storage capacity required depends upon the number of finite elements desired. As an example, the sample program presented in this paper having a total number of 6 elements requires a storage of 100 K for the evaluation of the stiffness and mass matrices of each element. These numbers are stored on a disk. In addition, a storage of 160 K, together with a time parameter of $2\frac{1}{2}$ minutes is required for the main program for a complete run. A typical element geometry and coordinate notation is given in figure 1. A geometrical element assembly is given in figure 2.

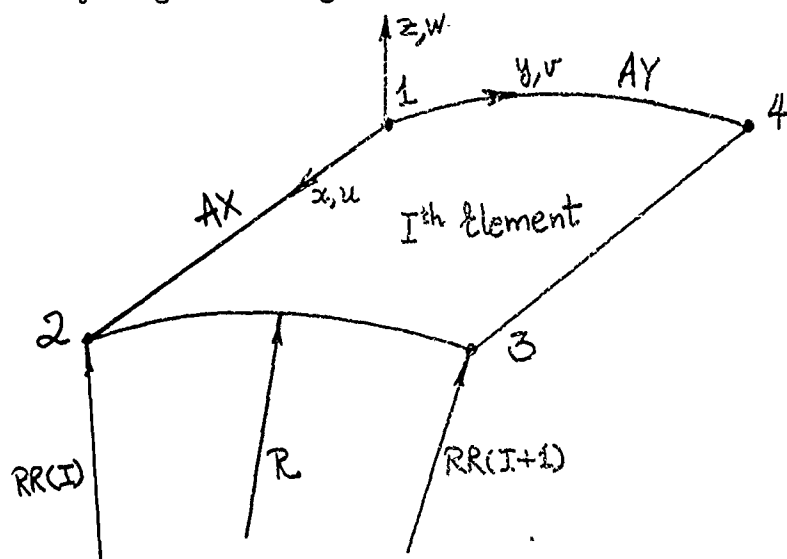


Figure 1. Individual finite element.

$$R = RR(I) + (RR(I+1) - RR(I)) \frac{Y}{AY}$$

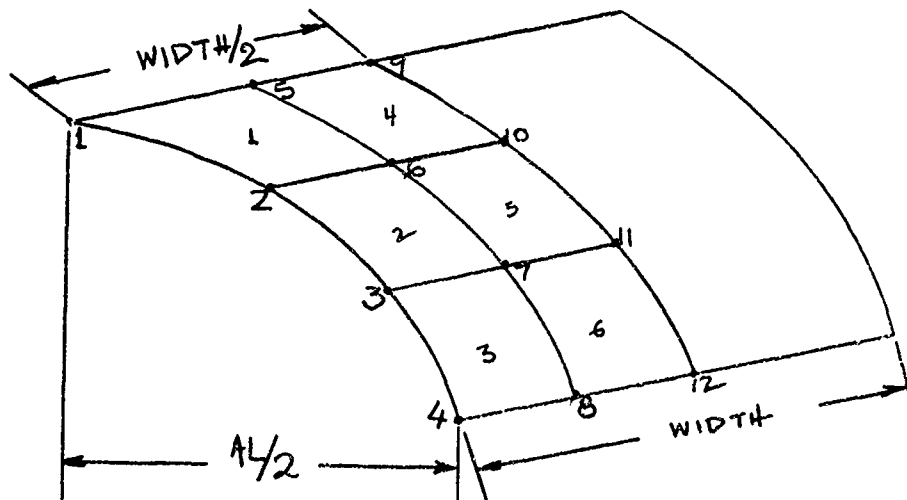


Figure 2. Finite element assembly of a shell.

Displacement vector δ_i per node is given as follows:

$$\delta_i = u_i, v_i, w_i, \frac{\partial u_i}{\partial x}, \frac{\partial v_i}{\partial x}, \frac{\partial w_i}{\partial x}, \frac{\partial u_i}{\partial y}, \frac{\partial v_i}{\partial y}, \frac{\partial w_i}{\partial y}$$

The program presented in Appendix A was written for the Class IV flextensional transducer shell, but it can be easily changed so it can be used for the case of any other similar type shell. Before using this particular program, it must be noted that all element stiffness and mass matrices are evaluated outside the main program. Then they are put on a disk from which the main program picks them up for total mass and stiffness formulation and final dynamic solution. It is necessary to use proper JCL cards. The program instruction in Appendix A must be read very carefully before running the program. A set of data cards is needed for the element notation and final mass and stiffness formulation. The program presented in Appendix A was written for figure 1. element notation and figure 2. element combination. All elements to form data for set 1. must be numbered according to figure 1 and figure 2.

ELEMENT NO. 1	5	1	2	6
ELEMENT NO. 4	9	5	6	10
ELEMENT NO. 2	6	2	3	7
ELEMENT NO. 5	10	6	7	11
ELEMENT NO. 3	7	3	4	8
ELEMENT NO. 6	11	7	8	12

SET 1

The boundary conditions are:

$$\begin{aligned}
 W_{y_i} &= 0 & i &= 1, 4, 5, 8, 9, 12 \\
 V_{z_i} &= 0 & i &= \text{"} \\
 V_{x_i} &= 0 & i &= \text{"} \\
 U_{z_i} &= 0 & i &= 9, 10, 11, 12 \\
 W_{y_i} &= 0 & i &= \text{"} \\
 W_{x_i} &= 0 & i &= \text{"}
 \end{aligned}$$

These are applied to the corresponding vector index notation

	u	v	w	u_x	v_x	w_x	u_y	v_y	w_y
Node 1	1	②	3	4	⑤	6	7	8	⑨
Node 2	10	11	12	13	14	15	16	17	18
Node 3	19	20	21	22	23	24	25	26	27
Node 4	28	②⑨	30	31	③②	33	34	35	③⑥
Node 5	37	③⑧	39	40	④①	42	43	44	④⑤
Node 6	46	47	48	49	50	51	52	53	54
Node 7	55	56	57	58	59	60	61	62	63
Node 8	64	⑥⑤	66	67	⑥⑧	69	70	71	⑦②
Node 9	⑦③	⑦④	75	76	⑦⑦	⑦⑧	⑦⑨	80	⑧①
Node 10	⑧②	83	84	85	86	⑧⑦	⑧⑧	89	90
Node 11	⑨①	92	93	94	95	⑨⑥	⑨⑦	98	99
Node 12	⑩①	⑩②	102	103	⑩④	⑩⑤	⑩⑥	107	⑩⑧

Therefore Set 3, corresponding to the total number of the above mentioned 30 boundary conditions (NBC=30), is easily formed as follows:

2 - 5 - 9 - 20 - 32 - 36 - 38 - 41	} SET 3
45 - 65 - 68 - 72 - 73 - 74 - 77 - 78	
79 - 81 - 82 - 87 - 88 - 91 - 96 - 97	
100 - 101 - 104 - 105 - 106 - 108	

In order to form Set 2, the vector index notation is used again, but the circled numbers that correspond to the boundary conditions are omitted.

Therefore, the vector index notation is as follows

Node 1	1 - (2) 3 - (4) 5 6 -
Node 2	(7) 8 9 10 11 12 13 14 15
Node 3	16 17 18 19 20 21 22 23 24
Node 4	25 - (26) 27 - (28) 29 30 -
Node 5	(31) - (32) 33 - (34) 35 36 -
Node 6	(37) 38 39 40 41 42 43 44 45
Node 7	46 47 48 49 50 51 52 53 54
Node 8	55 - (56) 57 - (58) 59 60 -
Node 9	- - (61) 62 - - - (63) -
Node 10	- (64) 65 66 - - - (68) 69
Node 11	- (70) 71 72 73 - - (74) 75
Node 12	- - (76) 77 - - - (78) - (79)

Then Set 2 is formed as follows:

2 - 4 - 7 - 26- 28- 31- 32- 34	}	SET 2
37- 56- 58- 61- 61- 61- 63- 63		
63- 64- 64- 68- 68- 70- 74- 74		
76- 76- 78- 78- 78- 79		

Then the data cards consist of Set 1- Set 2- Set 1- Set 3 in that order.

Furthermore if a coordinate transformation is desired, then matrix AKL (I,J), card MAIN 85, should be assigned properly and also cards DISK 27 and MAIN 266, 267, 268 should be removed from the program. In addition, card MAIN 54 should be equal to 1.

FINAL REMARKS

A 5 point numerical integration is carried out for each element's stiffness and mass matrix by using abscissas and weight functions of Legendre polynomials. After combining all the individual stiffness and mass matrices and introducing boundary conditions, the equation of motion for the shell is written as follows:

$$[[K] - \lambda [M]] \{ \delta \}^e = \{ 0 \}$$

where

$[K]$ = Total stiffness matrix

$[M]$ = Total mass matrix

$\{ \delta \}^e$ = Nodal vector

$$\lambda = E / (2 \cdot RHO \cdot (1 - POISS^2) \cdot \omega^2)$$

RHO = Density

E = Modulus of Elasticity

$POISS$ = Poisson's Ratio

Since subroutine NROOT is used to determine λ , the largest λ is determined first, and as a result, the lowest natural frequency is calculated first and so is the corresponding eigenvector.

10

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1. Larry H. Royster, " The Flextensional Concept: A New Approach to the Design of Underwater Transducers", Center for Acoustical Studies, Department of Mechanical and Aerospace Engineering, North Carolina State University, Raleigh, N. C., September, 1969.
2. Georgopoulos, George and L. H. Royster, "Development of a Finite Element Model for the Class IV Flextensional Underwater Transducer Shell", Technical Report No. 23, Department of Mechanical and Aerospace Engineering, North Carolina State University, Raleigh, N. C., September, 1972.

APPENDIX A

DIMENSION	AKK(36,36),AKL(36,36),AKM(36,36),BF(36,36),AA(5),H(5),RR	GSLG	2
1(4)		GSLG	3
C	AKK(NF,NF)	GSLG	4
C	AKL(NF,NF)	GSLG	5
C	AKM(NF,NF)	GSLG	6
C	BF(NF,NF)	GSLG	7
C	AA(NX)	GSLG	8
C	H(NX)	GSLG	9
C	RR(IMAX+1)	GSLG	10
C	IF NAK=1 THEN AKK(NF,NF)=STIFFNESS	GSLG	11
C	IF NAK=2 THEN AKK(NF,NF)=MASS	GSLG	12
C	D=E/(2*RH0*(1.0-POISS*POISS))	GSLG	13
C	RR(1)=RADIUS OF CURVATURE AT I TH NODE (IN), DIMENSION OF RR(I)=	GSLG	14
C	NUMBER OF ELEMENTS IN Y-DIRECTION+1	GSLG	15
	RR(1)=4.70	GSLG	16
	RR(2)=4.0	GSLG	17
	RR(3)=3.50	GSLG	18
	RR(4)=1.90	GSLG	19
	R1=RR(I)	GSLG	20
	R2=RR(I+1)	GSLG	21
	NX=5	GSLG	22
	NY=5	GSLG	23
	NZ=5	GSLG	24
	AA(1)=-0.90618	GSLG	25
	AA(2)=-0.538469	GSLG	26
	AA(3)=0	GSLG	27
	AA(4)=0.538469	GSLG	28
	AA(5)=0.90618	GSLG	29
	H(1)=0.236927	GSLG	30
	H(2)=0.478629	GSLG	31
	H(3)=0.568889	GSLG	32
	H(4)=0.478629	GSLG	33
	H(5)=0.236927	GSLG	34
	X1=0	GSLG	35
	X2=1	GSLG	36
	Y1=0	GSLG	37

38 GSLG
 39 GSLG
 40 GSLG
 41 GSLG
 42 GSLG
 43 GSLG
 44 GSLG
 45 GSLG
 46 GSLG
 47 GSLG
 48 GSLG
 49 GSLG
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 68 GSLG
 69 GSLG
 70 GSLG
 71 GSLG
 72 GSLG
 73 GSLG

```

Y2=1
Z1=-THICK/2.0
Z2=THICK/2.0
IF (NAK.EQ.2) GO TO 10
DO 1 J1=1,NF
DO 1 I1=J1,NF
AKK(I1,J1)=0
CONTINUE
DO 2 K1=1,NZ
Z=AA(K1)*(Z2-Z1)/2.0+(Z2+Z1)/2.0
DO 3 J1=1,NF
DO 3 I1=J1,NF
AKL(I1,J1)=0
CONTINUE
DO 4 K=1,NY
Y=AA(K)*(Y2-Y1)/2.0+(Y2+Y1)/2.0
DO 5 J1=1,NF
DO 5 I1=J1,NF
AKM(I1,J1)=0
CONTINUE
DO 6 L=1,NX
X=AA(L)*(X2-X1)/2.0+(X2+X1)/2.0
CALL FSTIF(MF,NF,AX,AY,PQISS,R1,R2,X,Y,Z,BF)
DO 7 J1=1,NF
DO 7 I1=J1,NF
AKM(I1,J1)=AKM(I1,J1)+H(L)*BF(I1,J1)
CONTINUE
CONTINUE
DO 8 J1=1,NF
DO 8 I1=J1,NF
AKL(I1,J1)=AKL(I1,J1)+H(K)*AKM(I1,J1)
CONTINUE
CONTINUE
DO 9 J1=1,NF
DO 9 I1=J1,NF
AKK(I1,J1)=AKK(I1,J1)+H(KL)*AKL(I1,J1)
  
```


9	CONTINUE	GSLG	74
2	CONTINUE	GSLG	75
10	GO TO 20	GSLG	76
	DO 11 J1=1,NF	GSLG	77
	DO 11 I1=J1,NF	GSLG	78
11	AKK(I1,J1)=0	GSLG	79
	CONTINUE	GSLG	80
	DO 12 K=1,NY	GSLG	81
	Y=AA(K)*((Y2-Y1)/2.0+(Y2+Y1)/2.0	GSLG	82
	DO 13 J1=1,NF	GSLG	83
	DO 13 I1=J1,NF	GSLG	84
	AKL(I1,J1)=0	GSLG	85
13	CONTINUE	GSLG	86
	DO 14 L=1,NX	GSLG	87
	X=AA(L)*((X2-X1)/2.0+(X2+X1)/2.0	GSLG	88
	CALL FMASS(MF,NF,AX,AY,R1,R2,X,Y,BF)	GSLG	89
	DO 15 J1=1,NF	GSLG	90
	DO 15 I1=J1,NF	GSLG	91
	AKL(I1,J1)=AKL(I1,J1)+H(L)*BF(I1,J1)	GSLG	92
15	CONTINUE	GSLG	93
14	CONTINUE	GSLG	94
	DO 16 J1=1,NF	GSLG	95
	DO 16 I1=J1,NF	GSLG	96
	AKK(I1,J1)=AKK(I1,J1)+H(K)*AKL(I1,J1)	GSLG	97
16	CONTINUE	GSLG	98
12	CONTINUE	GSLG	99
20	DO 19 I1=1,NF	GSLG	100
	DO 19 J1=I1,NF	GSLG	101
	AKK(I1,J1)=AKK(J1,I1)	GSLG	102
19	CONTINUE	GSLG	103
	RETURN	GSLG	104
	END	GSLG	105

C	SUBROUTINE FSTIF(MF,NF,AX,AY,POISS,R1,R2,X,Y,Z,BF)	1	STIF
C	DIMENSION DD(3,3),BB(3,36),BD(36,3),BF(36,36)	2	STIF
C	BR(MF,NF)	3	STIF
C	DD(MF,MF)	4	STIF
C	BD(MF,MF)	5	STIF
C	BF(NF,NF)	6	STIF
C	DD(MF,MF)=E/(1.0-POISS*POISS)*DD(MF,MF)	7	STIF
C	STIFF(NF,NF)=E/(1.0-POISS*POISS)*1/2*THICK*AX*AY*BF(NF,NF)	8	STIF
	R=21+(R2-R1)*Y	9	STIF
	DR=(R2-R1)/AY	10	STIF
	DD(1,1)=1	11	STIF
	DD(1,2)=POISS	12	STIF
	DD(1,3)=0	13	STIF
	DD(2,1)=POISS	14	STIF
	DD(2,2)=1	15	STIF
	DD(2,3)=0	16	STIF
	DD(3,1)=0	17	STIF
	DD(3,2)=0	18	STIF
	DD(3,3)=(1.0-POISS)/2.0	19	STIF
	BB(1,1)=(-Y-6*X+6*X*Y+3*Y*Y+6*X*X-6*X*X*Y-2*Y*Y*Y)/AX	20	STIF
	BB(2,1)=(-X-6*Y+3*X*X+6*X*Y+6*Y*Y-2*X*X*X-6*X*Y*Y)/AY	21	STIF
	BB(1,2)=0	22	STIF
	BB(2,2)=(1.0+Z/R)*(-X-6*Y+3*X*X+6*X*Y+6*Y*Y-2*X*X*X-6*X*Y*Y)/AY-Z*STIF	23	STIF
	1DR=(1.0-X*Y-3*X*X-3*Y*Y+3*X*X*Y+3*X*Y*Y+2*X*X*X+2*Y*Y*Y-2*X*X*X*Y-2*Y*Y*Y)/((R*R)	24	STIF
	12*X*Y*Y)/((R*R)	25	STIF
	BB(3,2)=(1.0+2*Z/R)*(-Y-6*X+6*X*Y+3*Y*Y+6*X*X-6*X*X*Y-2*Y*Y*Y)/AX	26	STIF
	BB(1,3)=-6*Z*(-1.0+Y+2*X-2*X*Y)/(AX*AX)	27	STIF
	BB(2,3)=(1.0-X*Y-3*X*X-3*Y*Y+3*X*X*Y+3*X*Y*Y+2*X*X*X+2*Y*Y*Y-2*X*X*X*Y-2*Y*Y*Y)	28	STIF
	1*X*Y-2*X*Y*Y)/R-6*Z*(-1.0+X+2*Y-2*X*Y)/(AX*AY)	29	STIF
	BB(3,3)=-2*Z*(-1.0+6*X+6*Y-6*X*X-6*Y*Y)/(AX*AY)	30	STIF
	BB(1,4)=1.0-Y-4*X+4*X*Y+3*X*X-3*X*X*Y	31	STIF
	BB(2,4)=0	32	STIF
	BB(3,4)=(-X+2*X*X-X*X*X)*AX/AY	33	STIF
	BB(1,5)=0	34	STIF
		35	STIF

```

36 RB(2,5)=(1.0+Z/R)*(-X+2*X*X-X*X*X)*AX/AY-Z*AX*DR*(X-X*Y-2*X*X+2*X*STIF
37 1X*Y+X*X*X-X*X*X*Y)/(R*R) STIF
38 RB(3,5)=(1.0+2*Z/R)*(1.0-Y-4*X+4*X*Y+3*X*X-3*X*X*Y) STIF
39 RB(1,6)=-Z*(-4.0+4*Y+6*X-6*X*Y)/AX STIF
40 RB(2,6)=AX*(X-X*Y-2*X*X+2*X*X*Y+X*X*X-X*X*X*Y)/R STIF
41 RB(3,6)=-2*Z*(-1.0+4*X-3*X*X)/AY STIF
42 RB(1,7)=AY*(-Y+2*Y*Y-Y*Y*Y)/AX STIF
43 RB(2,7)=0 STIF
44 RB(3,7)=1.0-X-4*Y+4*X*Y+3*Y*Y-3*X*Y*Y STIF
45 BE(1,8)=0 STIF
46 RB(2,8)=(1.0+Z/R)*(1.0-X-4*Y+4*X*Y+3*Y*Y-3*X*Y*Y)-Z*AY*DR*(Y-X*Y-2*STIF
47 1*Y*Y+2*X*Y*Y+Y*Y*Y-X*Y*Y*Y)/(R*R) STIF
48 RB(3,8)=AY*(1.0+2*Z/R)*(-Y+2*Y*Y-Y*Y*Y)/AX STIF
49 RB(1,9)=0 STIF
50 RB(2,9)=AY*(Y-X*Y-2*Y*Y+2*X*Y*Y+Y*Y*Y-X*Y*Y*Y)/R-Z*(-4.0+4*X+6*Y-6*STIF
51 1*X*Y)/AY STIF
52 RB(3,9)=-2*Z*(-1.0+4*Y-3*Y*Y)/AX STIF
53 RB(1,10)=(Y+6*X-6*X*Y-3*Y*Y-6*X*X+6*X*X*Y+2*Y*Y*Y)/AX STIF
54 RB(2,10)=0 STIF
55 RB(3,10)=(X-3*X*X-6*X*Y+2*X*X*X+6*X*Y*Y)/AY STIF
56 RB(1,11)=0 STIF
57 RB(2,11)=(1.0+Z/R)*(X-3*X*X-6*X*Y+2*X*X*X+6*X*Y*Y)/AY-Z*DR*(X*Y+3*STIF
58 1X*X-3*X*X*Y-3*X*Y*Y-2*X*X*X*X+2*X*X*X*Y+2*X*X*Y*Y*Y)/(R*R) STIF
59 RB(3,11)=(1.0+2*Z/R)*(Y+6*X-6*X*Y-3*Y*Y-6*X*X+6*X*X*Y+2*Y*Y*Y)/AX STIF
60 RB(1,12)=-6*Z*(1.0-Y-2*X+2*X*Y)/(AX*AX) STIF
61 RB(2,12)=(X*Y+3*X*X-X-3*X*X*Y-3*X*Y*Y-2*X*X*X+2*X*X*Y*Y)/RSTIF
62 1-6*Z*(-X+2*X*Y)/(AY*AY) STIF
63 RB(3,12)=-2*Z*(1.0-6*X-6*Y+6*X*X+6*Y*Y)/(AX*AY) STIF
64 RB(1,13)=-2*X+2*X*Y+3*X*X-3*X*X*Y STIF
65 RB(2,13)=0 STIF
66 RB(3,13)=(X*X-X*X*X)*AX/AY STIF
67 RB(1,14)=0 STIF
68 RB(2,14)=(1.0+Z/R)*(X*X-X*X*X)*AX/AY-Z*AX*DR*(-X*X+X*X*Y+X*X*X-X*X*STIF
69 1*X*Y)/(R*R) STIF
70 RB(3,14)=(1.0+2*Z/R)*(-2*X+2*X*Y+3*X*X-3*X*X*Y) STIF
71 RB(1,15)=-2*Z*(-1.0+Y+3*X-3*X*Y)/AX STIF

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BB(2,15) = (-X*X+X*X*Y+X*X*X-X*X*X*Y)*AX/R      STIF 72
BB(3,15) = -2*Z*(2*X-3*X*X)/AY                     STIF 73
BB(1,16) = (Y-2*Y*Y+Y*Y*Y)*AY/AX                  STIF 74
BB(2,16) = 0                                           STIF 75
BB(3,16) = X-4*X*Y+3*X*X*Y*Y                       STIF 76
BB(1,17) = 0                                           STIF 77
BB(2,17) = (1.0+Z/R)*(X-4*X*Y+3*X*X*Y*Y)-Z*AY*DR*(X*Y-2*X*Y*Y+X*Y*Y*Y) STIF 78
1/(R*R)                                                STIF 79
BB(3,17) = (1.0+2*Z/R)*(Y-2*Y*Y+Y*Y*Y)*AY/AX       STIF 80
BB(1,18) = 0                                           STIF 81
BB(2,18) = (X*Y-2*X*Y*Y+X*Y*Y*Y)*AY/R-Z*(-4*X+6*X*Y)/AY STIF 82
BB(3,18) = -2*Z*(1.0-4*Y+3*Y*Y)/AX                 STIF 83
BB(1,19) = (-Y+6*X*Y+3*Y*Y-6*X*X*Y-2*Y*Y*Y)/AX     STIF 84
BB(2,19) = 0                                           STIF 85
BB(3,19) = (-X+3*X*X+6*X*Y-2*X*X*X-6*X*Y*Y)/AY     STIF 86
BB(1,20) = 0                                           STIF 87
BB(2,20) = (1.0+Z/R)*(-X+3*X*X+6*X*Y-2*X*X*X-6*X*Y*Y)/AY-Z*DR*(-X*Y+STIF 88
13*X*X*Y+3*X*Y*Y-2*X*X*X*Y-2*X*Y*Y*Y)/(R*R)        STIF 89
BB(3,20) = (1.0+2*Z/R)*(-Y+6*X*Y+3*Y*Y-6*X*X*Y-2*Y*Y*Y)/AX STIF 90
BB(1,21) = -6*Z*(Y-2*X*Y)/(AX*AX)                  STIF 91
BB(2,21) = (-X*Y+3*X*X*Y+3*X*Y*Y-2*X*X*X*Y-2*X*Y*Y*Y)/R-6*Z*(X-2*X*YSTIF 92
1)/(AY*AY)                                             STIF 93
BB(3,21) = -2*Z*(-1.0+6*X+6*Y-6*X*X-6*Y*Y)/(AX*AY) STIF 94
BB(1,22) = -2*X*Y+3*X*X*Y                            STIF 95
BB(2,22) = 0                                           STIF 96
BB(3,22) = (-X*X+X*X*X)*AX/AY                       STIF 97
BB(1,23) = 0                                           STIF 98
BB(2,23) = (1.0+Z/R)*(-X*X+X*X*X)*AX/AY-Z*AX*DR*(-X*X*Y+X*X*X*Y)/(R*STIF 99
1R)                                                    STIF 100
BB(3,23) = (1.0+2*Z/R)*(-2*X*Y+3*X*X*Y)             STIF 101
BB(1,24) = -Z*(-2*Y+6*X*Y)/AX                       STIF 102
BB(2,24) = AX*(-X*X*Y+X*X*X*Y)/R                   STIF 103
BB(3,24) = -2*Z*(-2*X+3*X*X)/AY                    STIF 104
BB(1,25) = (-Y*Y+Y*Y*Y)*AY/AX                      STIF 105
BB(2,25) = 0                                           STIF 106
BB(3,25) = -2*X*Y+3*X*X*Y*Y                         STIF 107

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BB(1,26)=0
BB(2,26)=(1.0+Z/R)*(-2*X*Y+3*X*Y*Y)-Z*AY*DR*(-X*Y*Y+X*Y*Y*Y)/(R*R)
BB(3,26)=(1.0+2*Z/R)*(-Y*Y+Y*Y*Y)*AY/AX
BB(1,27)=0
BB(2,27)=(-X*Y*Y+X*Y*Y*Y)*AY/R-Z*(-2*X+6*X*Y)/AY
BB(3,27)=-2*Z*(-2*Y+3*Y*Y)/AX
BB(1,28)=(Y-6*X*Y-3*Y*Y+6*X*X*Y+2*Y*Y*Y)/AX
BB(2,28)=0
BB(3,28)=(X+6*Y-3*X*X-6*X*Y-6*Y*Y+2*X*X*X+6*X*Y*Y)/AY
BB(1,29)=0
BB(2,29)=(1.0+Z/R)*(X+6*Y-3*X*X-6*X*Y-6*Y*Y+2*X*X*X+6*X*Y*Y)/AY-Z/STIF
1(R*R)*(X*Y+3*Y*Y-3*X*X*Y-3*Y*Y*Y-2*Y*Y*Y+2*X*X*Y+2*X*Y*Y*Y)*DR
BB(3,29)=(1.0+2*Z/R)*(Y-6*X*Y-3*Y*Y+6*X*X*Y+2*Y*Y*Y)/AX
BB(1,30)=-6*Z*(-Y+2*X*Y)/(AX*AX)
BB(2,30)=(X*Y+3*Y*Y-3*X*X*Y-3*Y*Y*Y-2*Y*Y*Y+2*X*X*Y+2*X*Y*Y*Y)/RSTIF
1-6*Z*(1.0-X-2*Y+2*X*Y)/(AY*AY)
BB(3,30)=-2*Z*(1.0-6*X-6*Y+6*X*X+6*Y*Y)/(AX*AY)
BB(1,31)=Y-4*X*Y+3*X*X*Y
BB(2,31)=0
BB(3,31)=(X-2*X*X+X*X*X)*AX/AY
BB(1,32)=0
BB(2,32)=(1.0+Z/R)*(X-2*X*X+X*X*X)*AX/AY-Z*AX*DR*(X*Y-2*X*X*Y+X*X*Y*Y)
1X*Y)/(R*R)
BB(3,32)=(1.0+2*Z/R)*(Y-4*X*Y+3*X*X*Y)
BB(1,33)=-Z*(-4*Y+6*X*Y)/AX
BB(2,33)=(X*Y-2*X*X*Y+X*X*X*Y)*AX/R
BB(3,33)=-2*Z*(1.0-4*X+3*X*X)/AY
BB(1,34)=(Y*Y-Y*Y*Y)*AY/AX
BB(2,34)=0
BB(3,34)=-2*Y+2*X*Y+3*Y*Y-3*X*Y*Y
BB(1,35)=0
BB(2,35)=(1.0+Z/R)*(-2*Y+2*X*Y+3*Y*Y-3*X*Y*Y)-Z*AY*DR*(-Y*Y+X*Y*Y+Y*Y*Y)
1Y*Y*Y-X*Y*Y*Y)/(R*R)
BB(3,35)=(1.0+2*Z/R)*(Y*Y-Y*Y*Y)*AY/AX
BB(1,36)=0
BB(2,36)=(-Y*Y+X*Y*Y+Y*Y*Y-X*Y*Y*Y)*AY/R-Z*(-2.0+2*X+6*Y-6*X*Y)/AYSTIF

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STIF 108
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BB(3,36)=-2*Z*(2*Y-3*Y*Y)/AX
CALL GTPRD(BB,DD,BD,MF,NF,MF)
CALL GMPRD(BD,BB,8F,NF,MF,NF)
RETURN
END

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SUBROUTINE FMASS(MF,NF,AX,AY,R1,R2,X,Y,BF)
DIMENSION AN(3,36),AS(36,3),8F(36,36)
AN(MF,NF)
AS(NF,MF)
8F(NF,NF)
MASS(NF,NF)=RHO*THICK*AX*AY*BF(NF,NF)
DO 1 I1=1,MF
DO 1 J1=1,NF
AN(I1,J1)=G
1 CONTINUE
DO 2 I1=1,MF
II=I1-1
AN(I1+1,I1+1)=1.0-AX*Y-3*X*X-3*Y*Y+3*X*Y*Y+3*X*X*Y+2*X*Y*Y+2*X*Y*Y
12*X*X*Y-2*X*Y*Y
AN(I1+1,I1+4)=AX*(X-X*Y-2*X*X+2*X*X*Y+X*X*X-X*X*X*Y)
AN(I1+1,I1+7)=AY*(Y-X*Y-2*X*Y+2*X*Y*Y+Y*Y*Y-X*Y*Y*Y)
AN(I1+1,I1+10)=X*Y+3*X*X-3*X*X*Y-2*X*X*Y*Y-2*X*X*X*Y+2*X*Y*Y*Y
1*Y
AN(I1+1,I1+13)=AX*(-X*X+X*X*Y+X*X*X-X*X*X*Y)
AN(I1+1,I1+16)=AY*(X*Y-2*X*Y*Y+X*Y*Y*Y)
AN(I1+1,I1+19)=-X*Y+3*X*Y+3*X*Y*Y-2*X*X*X*Y-2*X*Y*Y*Y
AN(I1+1,I1+22)=AX*(-X*X*Y+X*X*X*Y)
AN(I1+1,I1+25)=AY*(-X*Y*Y+X*Y*Y*Y)
AN(I1+1,I1+28)=X*Y+3*Y*Y-3*X*X*Y-3*X*X*Y*Y-2*X*Y*Y+2*X*X*Y*Y
1*Y
AN(I1+1,I1+31)=AX*(X*Y-2*X*X*Y+X*X*X*Y)

MASS 27
MASS 28
MASS 29
MASS 30
MASS 31
MASS 32

AN(II+1,II+34)=AY*(-Y*Y+X*Y*Y+Y*Y*Y-X*Y*Y*Y)
2 CONTINUE
CALL GMTRA(AN,AS,MF,NF)
CALL GMPRD(AS,AN,BF,NF,MF,NF)
RETURN
END

1 DIMENSION AKK(36,36),AKL(36,36),AKM(36,36),AKN(36,36),A(78,78),RM(MAIN
2 178,78),ARA(78,78),VU(78),AKF(108,108)
3 INTEGER VC(30)
4 EQUIVALENCE (AKF(1),ARA(1)),(RM(1),AKK(1))
5 *****
6 PROGRAM WRITTEN BY GEORGE GEORGOPOULOS
7 *****
8 AKK(NF,NF)
9 AKL(NF,NF)
10 AKM(NF,NF)
11 AKN(NF,NF)
12 A(N,N)
13 RM(N,N)
14 ARA(N,N)
15 VU(N)
16 AKF(NPK,NPK)
17 VC(NBC)
18 NF=DEGREES OF FREEDOM PER ELEMENT
19 NM=NUMBER OF ELEMENTS IN X-DIRECTION (WIDTH)
20 NELEM=NUMBER OF ELEMENTS

C	NPOIN=NUMBER OF NODAL POINTS	21	MAIN
C	NFREE=DEGREES OF FREEDOM PER NODAL POINT	22	MAIN
C	NPK=NPOIN*NFREE	23	MAIN
C	NBC=NUMBER OF BOUNDARY CONTITIONS	24	MAIN
C	N=NPK-NBC	25	MAIN
C	AX=LENGTH OF THE ELEMENT IN X-DIRECTION (IN)	26	MAIN
C	AY=LENGTH OF THE ELEMENT IN Y-DIRECTION (IN)	27	MAIN
C	E=MODULUS OF ELASTICITY (LBF/IN**2)	28	MAIN
C	RHO=DENSITY (LBM/IN**3)	29	MAIN
C	POISS=POISSON'S RATIO	30	MAIN
C	THICK=THICKNESS (IN)	31	MAIN
C	AL=SHELL'S OPENNING LENGTH (IN)	32	MAIN
C	AX=0.75	33	MAIN
	AY=1.542	34	MAIN
	E=10300000	35	MAIN
	RHO=0.098	36	MAIN
	RHO=RHO/386.4	37	MAIN
	POISS=0.334	38	MAIN
	THICK=0.4	39	MAIN
	AL=6.60	40	MAIN
C	OMEGA=NATURAL FREQUENCY (RAD/SEC)	41	MAIN
C	FREQU=NATURAL FREQUENCY (CYCLES/SEC)	42	MAIN
C	COEF1=OMEGA#DI,FREQUENCY COEFFICIENT	43	MAIN
C	IF COORDINATE TRANSFORMATION IS DESIRED THEN AKL(I,J) IS THE	44	MAIN
C	DIRECTIONAL COSINE TRANSFORMATION MATRIX, THAT IS $K'=(AKL)T*K*(AKL)$	45	MAIN
C	D=E/(RHO*2*(1.0-POISS*POISS))	46	MAIN
C	OMEGA=SQRT(D/VU(I))	47	MAIN
C	COEF1=OMEGA#DI	48	MAIN
	NELEM=6	49	MAIN
	NPOIN=12	50	MAIN
	NBC=30	51	MAIN
	NM=2	52	MAIN
	NM1=1	53	MAIN
	NM2=NM	54	MAIN
	NFREE=9	55	MAIN
	NPK=NFREE*NPOIN	56	MAIN


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NF=4*NFREE
N=NPK-NBC
NN=N
D=E/(RHO*2*(1.0-POISS*POISS))
D1=AL*AL/THICK*SQRT((RHO*12)/E)
DO 1 I1=1,NF
DO 1 J1=1,NF
AKL(I1,J1)=0
1 CONTINUE
NAK=0
2 NAK=NAK+1
DO 3 I1=1,NPK
DO 3 J1=1,NPK
AKF(I1,J1)=0
3 CONTINUE
IJ=NELEM/NM
DO 43 I=1,IJ
IF (NAK.EQ.1) GO TO 5
INSERT MASS 'M'
READ (8,4) ((AKK(I1,J1),J1=1,NF),I1=1,NF))
4 FORMAT (/,4E15.7)
5 IF (NAK.GT.1) GO TO 6
INSERT 'STIFFNESS' MATRIX
READ (8,4) ((AKK(I1,J1),J1=1,NF),I1=1,NF))
6 DO 43 IR=1,NM1
IC=0
7 DO 9 ID=1,2
DO 8 IJK=1,NFREE
AKL(IJK+IC,IJK+IC)=1
8 CONTINUE
IC=IC+NFREE
9 CONTINUE
IF (IC.EQ.(2*NFREE)) GO TO 7
CALL GTPRD(AKL,AKK,AKN,NF,NF,NF)
CALL GMPRD(AKM,AKL,AKN,NF,NF,NF)
DO 43 IP=1,NM2

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READ (1,10) L,J,K,M
10 FORMAT (4I5)
   LL=L*NFREE
   JJ=J*NFREE
   KK=K*NFREE
   MM=M*NFREE
   LLL=LL-NFREE+1
   JJJ=JJ-NFREE+1
   KKK=KK-NFREE+1
   MMM=MM-NFREE+1
   LI=1
   DO 12 I1=LLL,LL
     M1=1
     DO 11 J1=LLL,LL
       AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
       M1=M1+1
11 CONTINUE
     LI=LI+1
12 CONTINUE
     LI=1
     DO 14 I1=LLL,LL
       M1=NFREE+1
       DO 13 J1=JJJ,JJ
         AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
         M1=M1+1
13 CONTINUE
       LI=LI+1
14 CONTINUE
       LI=1
       DO 16 I1=LLL,LL
         M1=2*NFREE+1
         DO 15 J1=KKK,KK
           AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
           M1=M1+1
15 CONTINUE
       LI=LI+1

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16	CONTINUE	MAIN 129
	L1=1	MAIN 130
	DO 18 I1=LLL,LL	MAIN 131
	M1=3*NFREE+1	MAIN 132
	DO 17 J1=MMM,MM	MAIN 133
	AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)	MAIN 134
	M1=M1+1	MAIN 135
17	CONTINUE	MAIN 136
	L1=L1+1	MAIN 137
18	CONTINUE	MAIN 138
	L1=NFREE+1	MAIN 139
	DO 20 I1=JJJ,JJ	MAIN 140
	M1=1	MAIN 141
	DO 19 J1=LLL,LL	MAIN 142
	AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)	MAIN 143
	M1=M1+1	MAIN 144
19	CONTINUE	MAIN 145
	L1=L1+1	MAIN 146
20	CONTINUE	MAIN 147
	L1=NFREE+1	MAIN 148
	DO 22 I1=JJJ,JJ	MAIN 149
	M1=NFREE+1	MAIN 150
	DO 21 J1=JJJ,JJ	MAIN 151
	AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)	MAIN 152
	M1=M1+1	MAIN 153
21	CONTINUE	MAIN 154
	L1=L1+1	MAIN 155
22	CONTINUE	MAIN 156
	L1=NFREE+1	MAIN 157
	DO 24 I1=JJJ,JJ	MAIN 158
	M1=2*NFREE+1	MAIN 159
	DO 23 J1=KKK,KK	MAIN 160
	AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)	MAIN 161
	M1=M1+1	MAIN 162
23	CONTINUE	MAIN 163
	L1=L1+1	MAIN 164

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24 CONTINUE
  L1=NFREE+1
  DO 26 I1=JJ,JJ
    M1=3*NFREE+1
    DO 25 J1=MM,MM
      AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
      M1=M1+1
    25 CONTINUE
    L1=L1+1
  26 CONTINUE
  L1=2*NFREE+1
  DO 28 I1=KKK,KK
    M1=1
    DO 27 J1=LLL,LL
      AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
      M1=M1+1
    27 CONTINUE
    L1=L1+1
  28 CONTINUE
  L1=2*NFREE+1
  DO 30 I1=KKK,KK
    M1=NFREE+1
    DO 29 J1=JJ,JJ
      AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
      M1=M1+1
    29 CONTINUE
    L1=L1+1
  30 CONTINUE
  L1=2*NFREE+1
  DO 32 I1=KKK,KK
    M1=2*NFREE+1
    DO 31 J1=KKK,KK
      AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
      M1=M1+1
    31 CONTINUE
    L1=L1+1

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32 CONTINUE
  L1=2*NFREE+1
  DO 34 I1=KK, KK
    M1=3*NFREE+1
    DO 33 J1=MM, MM
      AKF(I1, J1)=AKF(I1, J1)+AKN(L1, M1)
      M1=M1+1
    33 CONTINUE
    L1=L1+1
  34 CONTINUE
  L1=3*NFREE+1
  DO 36 I1=MM, MM
    M1=1
    DO 35 J1=LL, LL
      AKF(I1, J1)=AKF(I1, J1)+AKN(L1, M1)
      M1=M1+1
    35 CONTINUE
    L1=L1+1
  36 CONTINUE
  L1=3*NFREE+1
  DO 38 I1=MM, MM
    M1=NFREE+1
    DO 37 J1=JJ, JJ
      AKF(I1, J1)=AKF(I1, J1)+AKN(L1, M1)
      M1=M1+1
    37 CONTINUE
    L1=L1+1
  38 CONTINUE
  L1=3*NFREE+1
  DO 40 I1=MM, MM
    M1=2*NFREE+1
    DO 39 J1=KK, KK
      AKF(I1, J1)=AKF(I1, J1)+AKN(L1, M1)
      M1=M1+1
    39 CONTINUE
    L1=L1+1

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40 CONTINUE
   LI=3*NFREE+1
   DO 42 J1=MM,MM
   M1=3*NFREE+1
   DO 41 J1=MM,MM
   AKF(I1,J1)=AKF(I1,J1)+AKN(L1,M1)
   M1=M1+1
41 CONTINUE
   LI=LI+1
42 CONTINUE
43 CONTINUE
   IF (NAK.GT.1) GO TO 45
   READ (1,44) (VC(I1),I1=1,NBC)
44 FORMAT (8I10)
45 DO 46 I1=1,NBC
   LA=VC(I1)
   IN=NPK-LA-I1+1
   IF (IN.LE.0) GO TO 46
   DO 46 J1=1,IN
   LB=LA+1
   CALL RINT(AKF,NPK,NPK,LA,LB)
   CALL CINT(AKF,NPK,LA,LB)
   LA=LB
46 CONTINUE
   IF (NAK.GT.1) GO TO 48
   DO 47 I1=1,N
   DO 47 J1=1,N
   A(I1,J1)=AKF(I1,J1)
47 CONTINUE
   NM=NELEM
   NM1=1
   NM2=NELEM
   GO TO 2
48 DO 49 I1=1,N
   DO 49 J1=1,N
   RM(I1,J1)=AKF(I1,J1)

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49 CONTINUE
  WRITE (3,55)
  CALL NROOT(N,RM,A,VU,ARA)
  DO 50 I=1,NN
    OMEGA=SQRT(D/VU(I))
    FREQU=OMEGA/6.28
    COEF1=OMEGA*D1
    WRITE (3,53) I,VU(I),OMEGA,FREQU,COEF1
50 CONTINUE
  WRITE (3,55)
  READ (1,44) (VC(I1),I1=1,NBC)
  A1=0
  I1=1
  I2=1
  DO 52 I=1,NPK
    IF ((VC(I1)-I).EQ.0) GO TO 51
    WRITE (3,54) I,(ARA(I2,J2),J2=1,6)
    I2=I2+1
  GO TO 52
51 WRITE (3,54) I,A1,A1,A1,A1,A1,A1
  I1=I1+1
52 CONTINUE
53 FORMAT (1X,'I=',I3,2X,'VU(I)=' ,E13.6,2X,'OMEGA=' ,E13.6,2X,'FREQU=' ,E13.6,2X,'COEF1=' ,E13.6,2X,/)
54 FORMAT (1X,'I=',I3,6E20.6,/)
55 FORMAT (1H1)
  CALL EXIT
  END
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MAIN 300

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1	VU(I)= 0.745420E 00	UFGA= 0.41440E 04	FZQU= 0.120525E 04	CFI= 0.152249E 02
2	VU(I)= 0.777777E 00	UFGA= 0.470350E 04	FZQU= 0.440240E 04	CFI= 0.726874E 02
3	VU(I)= 0.440300E 00	UFGA= 0.440300E 04	FZQU= 0.440300E 04	CFI= 0.111099E 02
4	VU(I)= 0.222222E 00	UFGA= 0.303077E 04	FZQU= 0.120922E 04	CFI= 0.150500E 02
5	VU(I)= 0.745420E 00	UFGA= 0.445732E 04	FZQU= 0.153789E 04	CFI= 0.180709E 02
6	VU(I)= 0.222222E 00	UFGA= 0.205562E 04	FZQU= 0.159529E 04	CFI= 0.104244E 02
7	VU(I)= 0.145677E 00	UFGA= 0.115371E 04	FZQU= 0.124669E 04	CFI= 0.217052E 02
8	VU(I)= 0.070300E 00	UFGA= 0.146130E 04	FZQU= 0.232691E 04	CFI= 0.273547E 02
9	VU(I)= 0.745420E 00	UFGA= 0.172419E 04	FZQU= 0.276462E 04	CFI= 0.225004E 02
10	VU(I)= 0.520534E 00	UFGA= 0.200541E 04	FZQU= 0.333231E 04	CFI= 0.289300E 02
11	VU(I)= 0.420856E 00	UFGA= 0.215782E 04	FZQU= 0.342603E 04	CFI= 0.403924E 02
12	VU(I)= 0.445101E 00	UFGA= 0.225113E 04	FZQU= 0.358460E 04	CFI= 0.421400E 02
13	VU(I)= 0.222222E 00	UFGA= 0.263077E 04	FZQU= 0.420346E 04	CFI= 0.494152E 02
14	VU(I)= 0.222222E 00	UFGA= 0.268074E 04	FZQU= 0.428302E 04	CFI= 0.503505E 02
15	VU(I)= 0.222222E 00	UFGA= 0.283061E 04	FZQU= 0.452167E 04	CFI= 0.531560E 02
16	VU(I)= 0.222222E 00	UFGA= 0.301509E 04	FZQU= 0.480109E 04	CFI= 0.564409E 02
17	VU(I)= 0.240032E 00	UFGA= 0.302947E 04	FZQU= 0.482400E 04	CFI= 0.557102E 02
18	VU(I)= 0.222222E 00	UFGA= 0.313352E 04	FZQU= 0.498969E 04	CFI= 0.536580E 02
19	VU(I)= 0.187271E 00	UFGA= 0.249348E 04	FZQU= 0.555287E 04	CFI= 0.653962E 02
20	VU(I)= 0.160574E 00	UFGA= 0.277156E 04	FZQU= 0.600569E 04	CFI= 0.706017E 02
21	VU(I)= 0.142857E 00	UFGA= 0.339897E 04	FZQU= 0.634709E 04	CFI= 0.746153E 02
22	VU(I)= 0.122782E 00	UFGA= 0.412328E 04	FZQU= 0.659166E 04	CFI= 0.773729E 02

I= 1	-0.511354E-01	0.144208E-02	-0.461120E-01	0.204674E-02	0.124910
I= 2	0.0	0.0	0.0	0.0	0.0
I= 3	-0.24474E 00	0.260975E 00	0.269269E 00	-0.329109E 00	-0.147391
I= 4	0.70'005E-02	0.624103E-03	-0.285640E-01	0.235794E-01	0.736192
I= 5	0.0	0.0	0.0	0.0	0.0
I= 6	-0.226221E-01	0.724584E-01	0.142047E-01	-0.510628E 00	-0.268741
I= 7	0.147719E-02	-0.994164E-03	-0.219148E-03	0.192991E-04	0.771892
I= 8	0.713418E-01	-0.607490E-01	0.274764E-01	0.598096E-02	0.122499
I= 9	0.0	0.0	0.0	0.0	0.0
I= 10	0.689724E-04	0.111425E-02	-0.442602E-01	0.242552E-02	0.515432
I= 11	0.101214E 00	-0.372622E-01	0.469012E-01	0.636452E-02	0.191855
I= 12	-0.201793E 00	-0.138359E 00	0.195061E 00	-0.250002E 00	0.119292
I= 13	0.461195E-02	0.974450E-03	-0.272910E-01	0.196465E-01	-0.254577
I= 14	0.144975E-01	-0.105195E-02	-0.255779E-02	0.251467E-02	0.117926
I= 15	-0.170269E-01	-0.334045E-01	-0.121244E-01	-0.296785E 00	0.220991
I= 16	0.209009E-02	-0.875294E-02	0.225516E-02	-0.217588E-02	-0.920223
I= 17	0.496620E-01	0.324711E-01	0.242667E-01	0.452245E-02	0.442079
I= 18	0.169253E 00	-0.309753E 00	-0.211268E-01	0.102541E 00	0.225245
I= 19	0.170692E-02	0.191035E-02	-0.292087E-01	-0.264074E-02	-0.427295
I= 20	0.121807E 00	0.536730E-01	0.796961E-01	0.851474E-02	0.145415
I= 21	0.971179E-01	-0.171569E 00	0.242556E 00	-0.941773E-01	0.264505
I= 22	-0.318769E-02	0.135632E-02	-0.244819E-01	0.999245E-02	-0.239499
I= 23	0.206004E-01	0.252534E-02	-0.244586E-02	0.426145E-02	0.277955
I= 24	0.137902E-01	-0.414297E-01	-0.721484E-02	-0.149207E 00	0.238701
I= 25	0.401601E-02	0.292951E-02	0.271272E-02	-0.235479E-02	-0.139444

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I= 24	-0.240912E-01	0.444813E-01	-0.772350E-01	-0.712422E-01	-0.752228
I= 27	0.190920E 00	0.277873E 00	0.948093E-01	0.102220E 00	0.753862
I= 28	0.616206E-05	0.239645E-02	-0.358255E-01	-0.607156E-02	-0.121240
I= 29	0.0	0.0	0.0	0.0	0.0
I= 30	0.262605E 00	0.220764E 00	0.240115E 00	-0.100711E-01	0.262250
I= 31	-0.949664E-01	0.123843E-02	-0.226702E-01	0.499287E-02	-0.292238
I= 32	0.0	0.0	0.0	0.0	0.0
I= 33	0.275546E-01	0.652267E-01	0.571091E-02	-0.252292E-01	0.411535
I= 34	0.107992E-02	0.140997E-02	-0.228075E-02	-0.2963913E-04	-0.234071
I= 35	-0.126700E 00	-0.127073E 00	-0.119604E 00	-0.758896E-02	-0.242965
I= 36	0.0	0.0	0.0	0.0	0.0
I= 37	-0.157473E-02	0.547172E-02	-0.237228E-01	-0.507322E-02	0.812021
I= 38	0.0	0.0	0.0	0.0	0.0
I= 39	-0.328222E 00	0.231437E 00	0.242573E 00	0.225859E-01	0.250532
I= 40	-0.154778E-02	0.108153E-02	-0.210097E-01	-0.261949E-03	0.971761
I= 41	0.0	0.0	0.0	0.0	0.0
I= 42	-0.100790E-01	0.151346E-01	0.192275E-02	-0.413990E 00	-0.223421
I= 43	-0.415600E-04	0.7738220E-04	0.145039E-04	0.255080E-02	-0.896541
I= 44	0.700224E-01	-0.578107E-01	0.201067E-01	-0.199895E-02	-0.000001
I= 45	0.0	0.0	0.0	0.0	0.0
I= 46	-0.284910E-01	0.574603E-02	-0.226000E-01	-0.425286E-02	0.520021
I= 47	0.100762E 00	-0.358824E-01	0.405554E-01	-0.200210E-01	-0.720211
I= 48	-0.100703E 00	-0.127046E 00	0.100722E 00	0.244042E-01	-0.966512
I= 49	-0.257246E-01	0.656213E-02	-0.207639E-01	-0.222627E-02	0.26077
I= 50	0.0	-0.100220E-01	-0.100220E-01	0.55422E-01	0.42001

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I= 52	0 120516E-03	-0.202490E-03	0.126228E-02	-0.387125E-03	-0.4047
I= 53	0.482510E-01	0.320986E-01	0.345012E-01	-0.157288E-02	0.74848
I= 54	0 162276E 00	-0.202280E 00	-0.272545E-01	-0.964545E-02	-0.19216
I= 55	0.165201E-03	0.071168E-03	-0.200715E-01	-0.524774E-02	0.43185
I= 56	0 121068E 00	0.528291E-01	0.803750E-01	-0.313767E-02	-0.54092
I= 57	0.014364E-01	-0.155985E 00	0.266885E 00	0.918327E-02	-0.16994
I= 58	0 202765E-03	0.122618E-02	-0.262489E-01	-0.202461E-02	-0.52020
I= 59	0.100782E-02	0.126573E-02	-0.131743E-02	0.192245E-01	0.35582
I= 60	0.320144E-02	-0.832931E-02	-0.426000E-02	-0.116914E 00	0.32707
I= 61	0.167231E-03	0.636171E-03	0.102123E-02	-0.125956E-02	0.18265
I= 62	-0 263142E-01	0.464457E-01	-0.279500E-02	0.120569E-02	0.11390
I= 63	0.175424E 00	0.265502E 00	0.831211E-01	-0.804466E-02	-0.34014
I= 64	0.107482E-02	0.866874E-02	-0.183520E-01	-0.642865E-02	0.23132
I= 65	0.0 0.0	0.0	0.0	0.0	0.0
I= 66	0 252026E 00	0.109793E 00	0.339934E 00	0.152033E-02	-0.29057
I= 67	0 172100E-02	0.155521E-02	-0.240014E-01	-0.474317E-02	-0.47477
I= 68	0.0 0.0	0.0	0.0	0.0	0.0
I= 69	0.550460E-02	0.717448E-02	-0.252409E-02	-0.148776E-01	0.32514
I= 70	-0.102572E-03	-0.276675E-02	-0.707407E-04	-0.252719E-02	-0.11203
I= 71	-0.134202E 00	-0.120816E 00	-0.111674E 00	0.315109E-02	0.10510
I= 72	0.0 0.0	0.0	0.0	0.0	0.0
I= 73	0.0 0.0	0.0	0.0	0.0	0.0
I= 74	0.0 0.0	0.0	0.0	0.0	0.0
I= 75	-0.22515E-01	0.22775E 00	0.242908E 00	0.315400E 00	0.10510

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I = 77	0 0	0 0	0 0	0 0	0 0	0 0
I = 78	0 0	0 0	0 0	0 0	0 0	0 0
I = 79	0 0	0 0	0 0	0 0	0 0	0 0
I = 80	0 707197E-01	-0 565680E-01	0 207340E-01	-0 430358E-02	-0 22455	-0 22455
I = 81	0 0	0 0	0 0	0 0	0 0	0 0
I = 82	0 0	0 0	0 0	0 0	0 0	0 0
I = 83	0 100407E 00	-0 751578E-01	0 401713E-01	-0 967730E-02	-0 26257	-0 26257
I = 84	-0 191724E 00	-0 125808E 00	0 700774E 00	0 152594E 00	-0 10610	-0 10610
I = 85	-0 619427E-04	0 846033E-03	-0 705000E-01	-0 879239E-02	0 822407	0 822407
I = 86	-0 739447E-05	0 111222E-02	0 164186E-03	-0 562333E-03	-0 19300	-0 19300
I = 87	0 0	0 0	0 0	0 0	0 0	0 0
I = 88	0 0	0 0	0 0	0 0	0 0	0 0
I = 89	0 490570E-01	0 317931E-01	0 247159E-01	-0 543733E-02	-0 42509	-0 42509
I = 90	0 160474E 00	-0 296519E 00	-0 256677E-01	-0 724159E-01	-0 17077	-0 17077
I = 91	0 0	0 0	0 0	0 0	0 0	0 0
I = 92	0 120628E 00	0 523582E-01	0 308527E-01	-0 113754E-01	-0 20270	-0 20270
I = 93	0 904430E-01	-0 153317E 00	0 768577E 00	0 555976E-01	-0 15300	-0 15300
I = 94	0 240105E-01	0 146720E-02	-0 269670E-01	-0 939696E-02	0 99437	0 99437
I = 95	-0 273220E-02	-0 112404E-02	0 472213E-04	-0 153076E-02	-0 61805	-0 61805
I = 96	0 0	0 0	0 0	0 0	0 0	0 0
I = 97	0 0	0 0	0 0	0 0	0 0	0 0
I = 98	-0 268564E-01	0 456509E-01	-0 303172E-02	0 349947E-02	0 49849	0 49849
I = 99	0 174229E 00	0 261630E 00	0 827827E-01	-0 695375E-01	-0 35691	-0 35691
I = 100	0 0	0 0	0 0	0 0	0 0	0 0

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I=101	0 0	0 0	0 0	0 0	0 0
I=102	0 250047F 00	0 109069F 00	0 341201F 00	0 652000F 02	-0 16261F
I=103	0 111142F 02	0 885035F 02	-0 247205F 01	-0 104523F 01	0 70586F
I=104	0 0	0 0	0 0	0 0	0 0
I=105	0 0	0 0	0 0	0 0	0 0
I=106	0 0	0 0	0 0	0 0	0 0
I=107	-0 134224F 00	-0 119046F 00	-0 112071F 00	0 103087F 01	0 32270
I=108	0 0	0 0	0 0	0 0	0 0